Q1.

Solution Let us consider the two corner voltages V_1 and V_1 that appear on the positive side of the waveform indicated in Fig. 2.8. This waveform represents the response of the high-pass filter when RC is very large compared to T. We can write that

$$V_{1}' = V_{1}e^{-T/2RC}$$

$$V_{2}' = V_{2}e^{-T/2RC}$$

$$V_{1} - V_{2}' = V$$

$$V_{1}' - V_{2} = V$$
(1)

We can write another two equations due to the symmetry of the waveform.

$$V_1 = -V_2$$
 and $V_1' = -V_2'$
 $V_1 - V_2' = V$

Substituting for V_2' , we have

$$V_{1} - V_{2}e^{-T/2RC} = V$$

$$V_{1} - (V_{1}' - V)e^{-T/2RC} = V$$

$$V_{1} - (V_{1}e^{-T/2RC} - V)e^{-T/2RC} = V$$

$$V_{1}(1 - e^{-T/RC}) = V(1 - e^{-T/2RC})$$

When $x \ll 1$, we can write $e^{-x} \approx (1-x)$ and $(1-x)^{-1} \approx (1+x)$. This relationship can be used when $T/2RC \ll 1$.

We can write

$$V_1 = \frac{V(1 - e^{-T/2RC})}{(1 - e^{-T/RC})} = \frac{V}{(1 + e^{-T/2RC})}$$
(2)

Similarly we can also obtain that

$$V_1' = V_1 e^{-T/2 RC} = \frac{V e^{-T/2 RC}}{(1 + e^{-T/2 RC})} = \frac{V}{(1 + e^{+T/2 RC})}$$
(3)

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(a)
$$V_1' = V_1 e^{-T_1/RC} = V_1 e^{-0.1/0.2} = 0.606V_1$$

 $V_2 = V_1' - V = V_1' - 1 = 0.606V_1 - 1$
 $V_2' = V_2 e^{-T_2/RC} = V_2 e^{-0.2/0.2} = 0.367V_2$
 $V_1 = V_2' + V = V_2' + 1 = 0.367V_2 + 1$

We obtain the following values by solving the four equations.

$$V_1 = 0.816 \text{ V}, V_1' = 0.496 \text{ V}, V_2 = -0.504 \text{ V} \text{ and } V_2' = -0.184 \text{ V}.$$

(b) Let positive area be A_1 , and negative area be A_2 .

$$A_1 = \int_0^{0.1} 0.816 e^{-t/0.2} dt = (-0.816(0.2) e^{-t/0.2})_0^{0.1} = 0.06 \text{ V-s}$$

$$A_1 = \int_0^{0.1} 0.816 e^{-t/0.2} dt = (-0.816(0.2)e^{-t/0.2})_0^{0.1} = 0.06 \text{ V-s}$$

$$A_2 = \int_0^{0.2} (-0.504) e^{-t/0.2} dt = (0.504(0.2)e^{-t/0.2})_0^{0.2} = -0.06 \text{ V-s}$$

$$A_1 + A_2 = 0.06 + (-0.06) = 0$$

The net area is obviously zero. This means that the series capacitor blocks the dc component of the inpu waveform.

Q3.

Solution The peak-to-peak amplitude of the symmetrical square-wave V is given as 2 V. We know that for a symmetrical square-wave, the average value is zero.

The waveform is transmitted through an RC low-pass filter. The rising portion of the output waveform is given by Eq. (2.52).

$$v_{o1}(t) = V' + (V_1 - V')e^{-t/RC}$$
(1)

We are dealing with a symmetrical square-wave with zero average value. We are given that V' = -V'' = 1 V. Let us assume that $T_1 = T_2 = t_p$. Substituting this in Eq. (1), we have

$$V = 1 + (-1 - V)e^{-t_p/RC}$$

$$V = 1 + (-1 - V)e^{-1} = 1 - (1 + V)(0.368)$$

$$1.368V = 0.632$$

 $V = \frac{0.632}{1.368} = 0.463 \text{ V}$

Peak-to-peak voltage of the output is 2V that is equal to $v_a \text{ (peak)} = 2V = 2 \times 0.463 = 0.926 \text{ V}$

Solution In the case of a symmetrical square waveform, we have $T_1 = T_2 = T/2$ and V' = -V'' = V/2. We also observe that $V_1 = -V_2$ due to symmetry. Substituting these values in Eqs (2.52) and (2.53), we can write

$$V_2 = \frac{V}{2} + \left(V_1 - \frac{V}{2}\right)e^{-T/2RC}$$

Since we know that $V_1 = -V_2$, we can write

$$V_2 = \frac{V}{2} + \left(-V_2 - \frac{V}{2}\right)e^{-T/2RC}$$

$$V_2(1 + e^{-T/2RC}) = \frac{V}{2}(1 - e^{-T/2RC})$$

$$V_2 = \frac{V(1 - e^{-T/2RC})}{2(1 + e^{-T/2RC})}$$

Multiplying the numerator and denominator in the above equation with $e^{T/2RC}$, we have

$$V_2 = \frac{V}{2} \frac{(e^{T/2RC} - 1)}{(e^{T/2RC} + 1)}$$

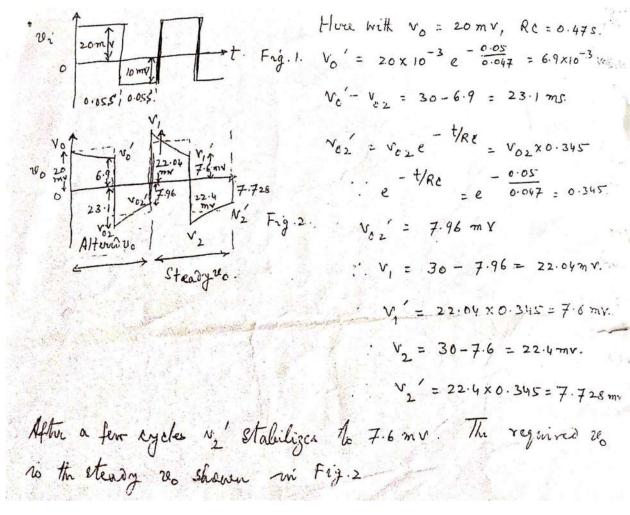
If we introduce x = T/4RC, the above equation assumes a simple form as

$$V_2 = \frac{V}{2} \frac{(e^{2x} - 1)}{(e^{2x} + 1)}$$

$$V_2 = \frac{V(e^x - e^{-x})}{2(e^x + e^{-x})}$$

$$V_2 = \frac{V(e^x - e^{-x})/2}{2(e^x + e^{-x})/2} = \frac{V \sinh x}{2 \cosh x}$$

$$V_2 = \frac{V}{2} \tanh x$$



Q6. & Q7 These are theoretical questions (Given in the Book Milliman & Taub)